

## Context

- **Lubricants = Industrial Fluids = Complex Materials**

⇒ **Structure – Properties Relationship Issue**

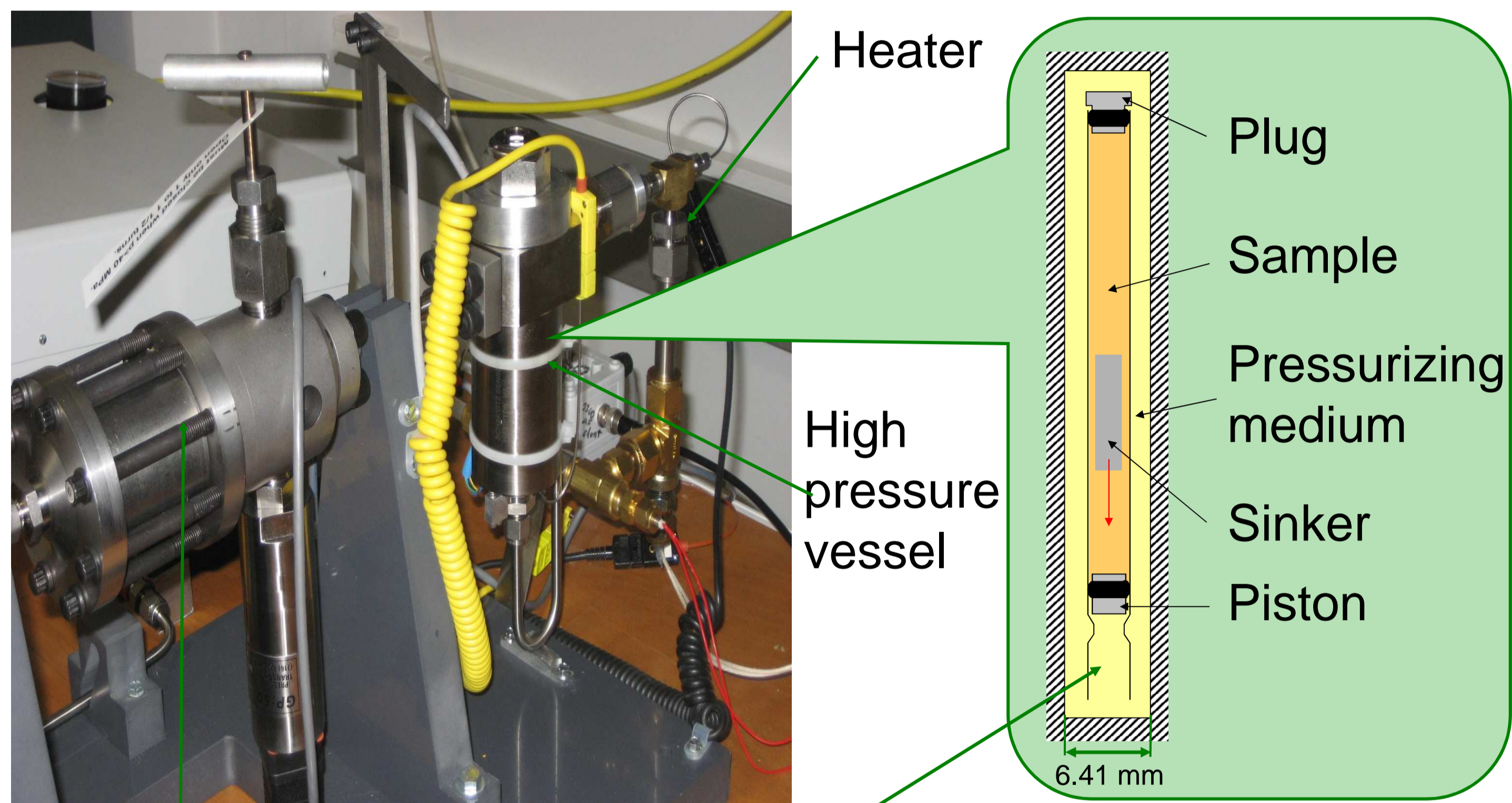
- **Rheological characterization:** rheometers

$$\eta = f(T, \dot{\gamma} \text{ or } \tau)$$

**high pressure viscometer**

$$\eta = f(T, P)$$

## High Pressure Viscometer



- **Falling body viscometer**

- Linear Variable Differential Transformer, LVDT, to monitor continuously the position of the sinker

- Different sinkers (solid, hollow or cup)

- $T : 0 \text{ to } 150^\circ\text{C}$

- $P : 0.1 \text{ to } 800 \text{ MPa}$

- $\eta : 2 \cdot 10^{-4} \text{ to } > 10^3 \text{ Pa}\cdot\text{s}$

Pressure intensifier

Cartridge placed in the vessel

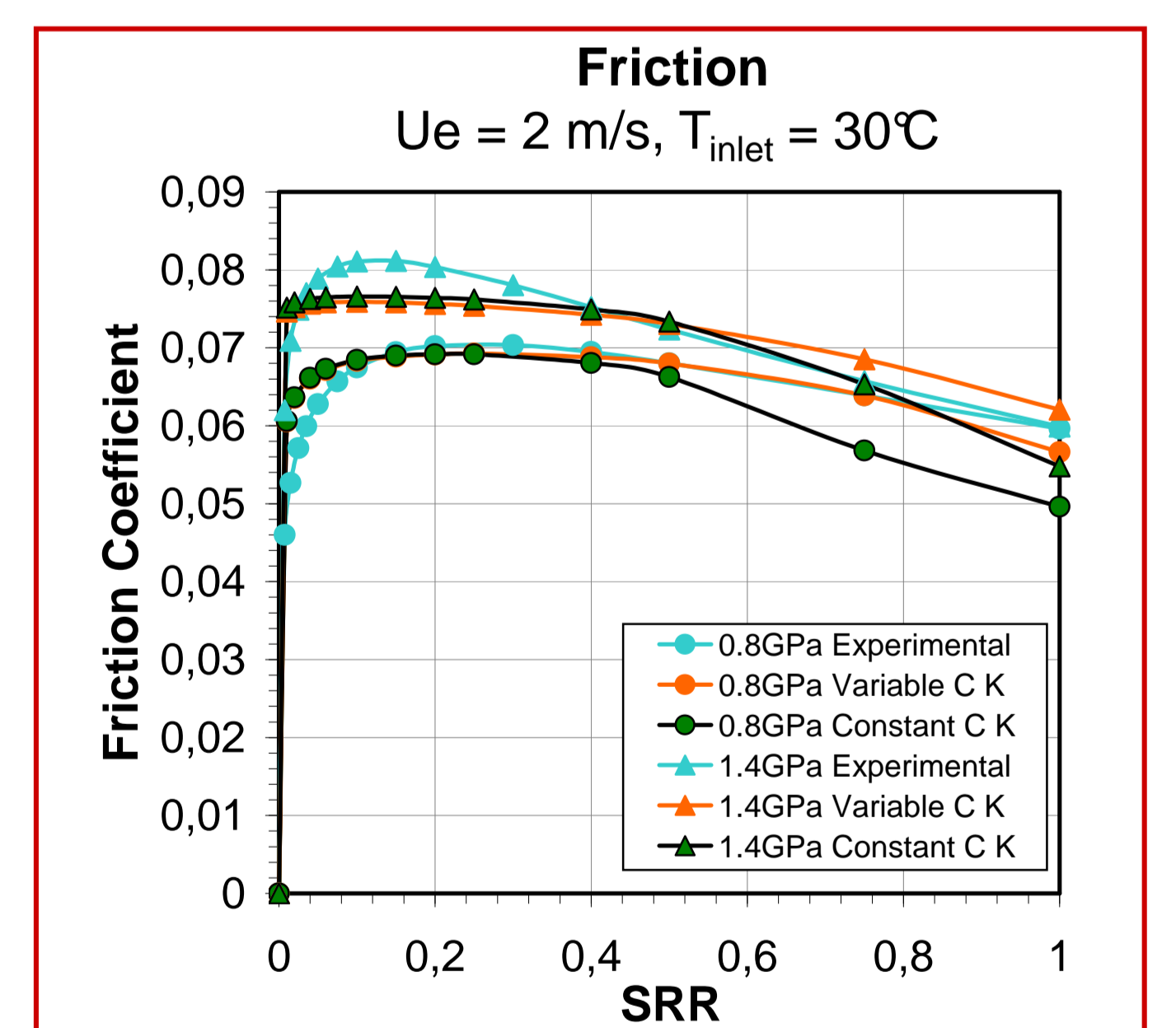
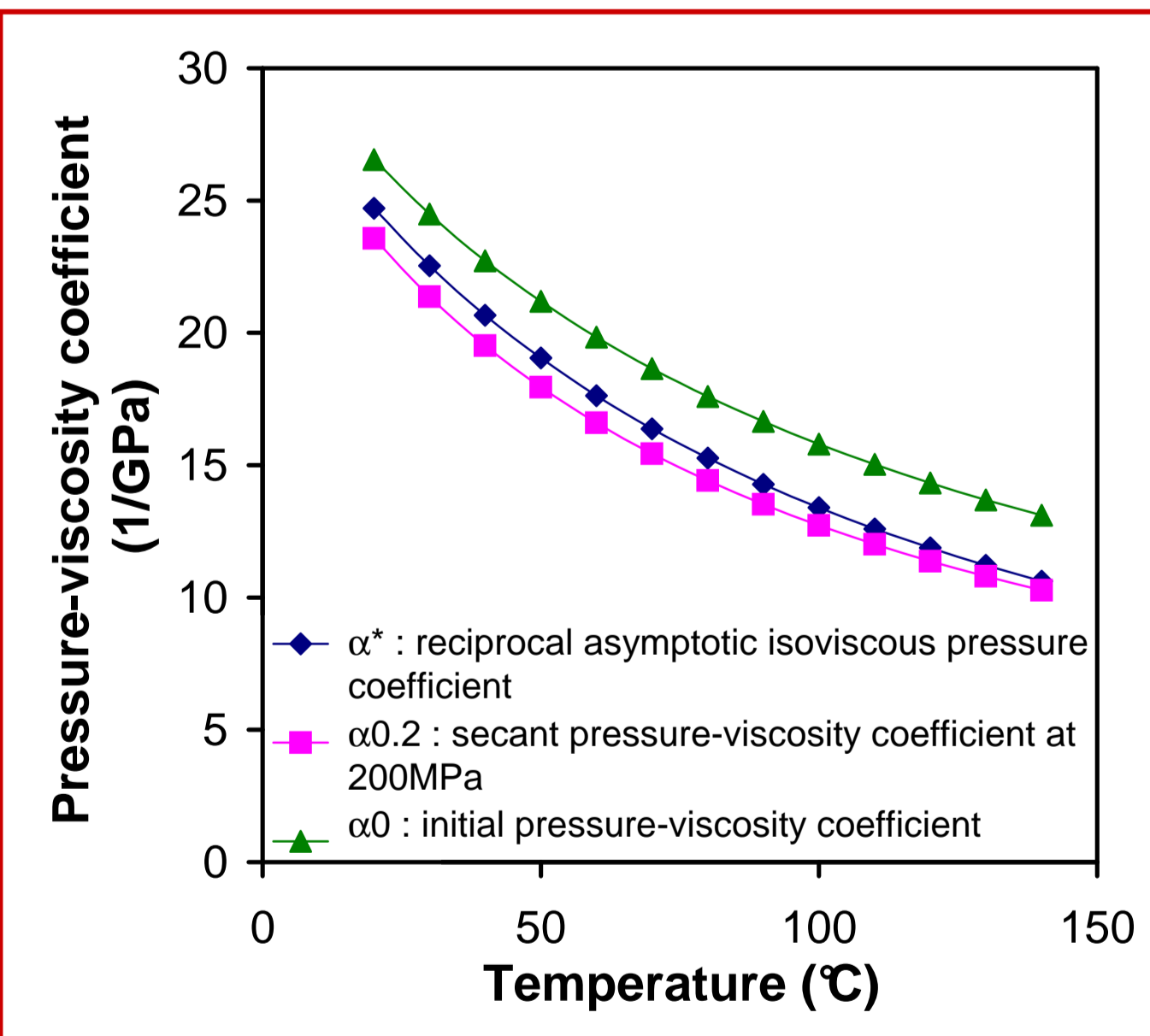
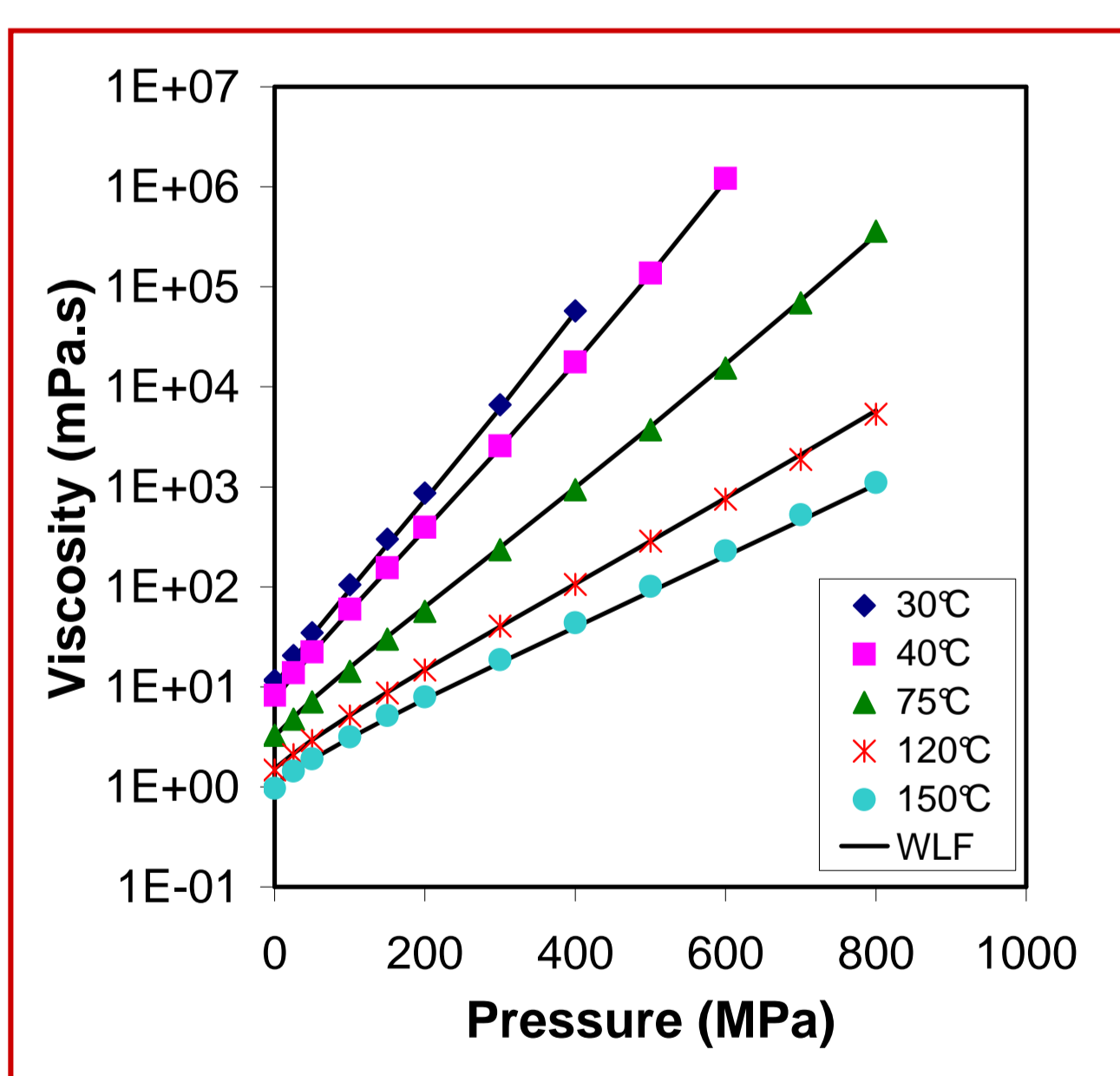
## Applications and objectives

Temperature – Pressure – Viscosity Response of lubricants

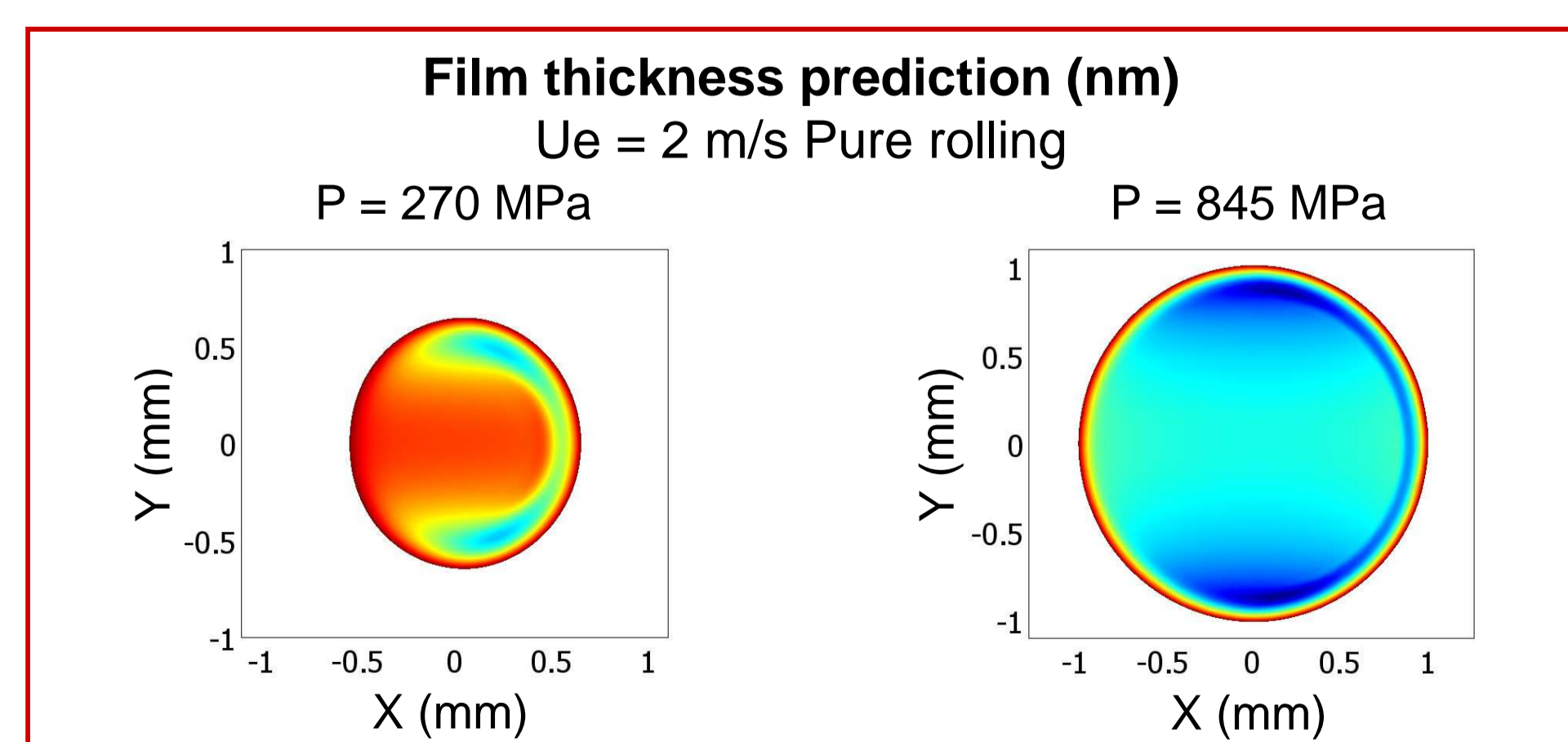
⇒  $\eta(P, T, \dot{\gamma})$  modeling

⇒ **Determination of lubrication regime**

⇒ **Film thickness and friction prediction from multiphysics models**



**Modelling using modified W. L. F. equation**  
 S. Bair, C. Mary, N. Bouscharain and P. Vergne, "An improved Yasutomi correlation for viscosity at high pressure", Proc IMechE Part J: J Engineering Tribology, 227(9) 1056–1060, 2013  
 $\log \mu = \log \mu_g - [C1 \cdot (T - T_g(P)) \cdot F(P)] / [C2 + (T - T_g(P)) \cdot F(P)]$   
 with  
 $T_g(P) = T_g(0) + A1 \cdot \ln(1 + A2 \cdot P)$ ,  $\mu_g = 10^{12} \text{ Pa}\cdot\text{s}$   
 $F(P) = (1 + b1 \cdot P)^{b2}$   
**7 parameters to determine**



**Case study with a mineral oil**