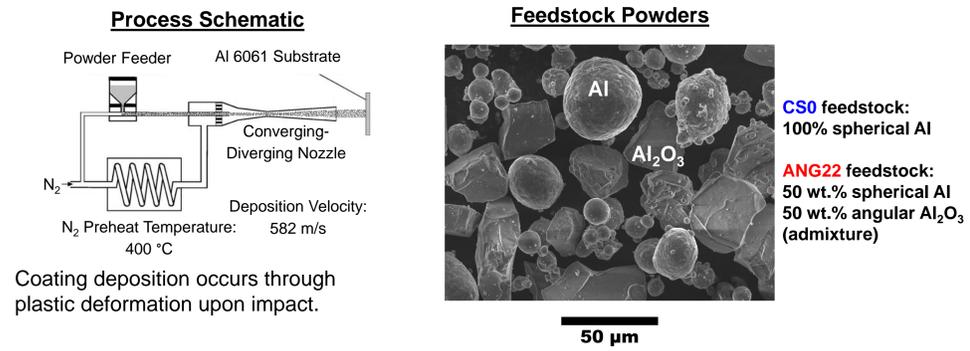


## INTRODUCTION

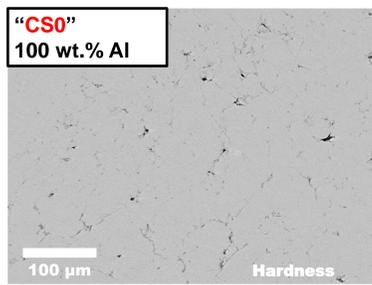
Particle-reinforced aluminum matrix composites (Al-MMCs) generally exhibit lower wear rates and more stable friction than their un-reinforced matrix materials [1]. Cold spray is a popular consolidation route for Al-Al<sub>2</sub>O<sub>3</sub>, allowing for its application as a coating for corrosion and tribological protection. Previous work by the authors has found that **22 wt.% of angular Al<sub>2</sub>O<sub>3</sub>** particles leads to significantly lower wear rates and greater friction stability compared to unreinforced **pure Al** cold sprayed coatings (see figures below) [2,3].

Characterization of the material present in the wear tracks is challenging. Third body layers may be only a few microns thick, and contain metastable / nanocrystalline / amorphous material. In this study, TEM methods were used to characterize the third body material of **pure Al** and **Al-22 wt.% Al<sub>2</sub>O<sub>3</sub>** cold spray coatings. In doing so, a mechanistic explanation of the contrasting dry sliding wear behavior of the two samples can be derived by describing the material transformations occurring at the sliding interface, which are dependent on the presence of Al<sub>2</sub>O<sub>3</sub> particles.

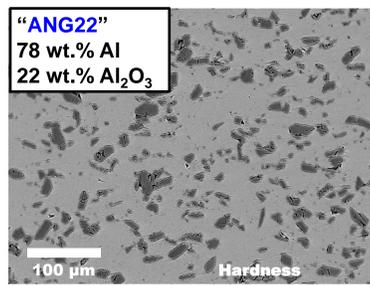
## COLD SPRAY DEPOSITION OF Al AND Al-Al<sub>2</sub>O<sub>3</sub>



## MATERIALS STUDIED: Al AND Al-Al<sub>2</sub>O<sub>3</sub>

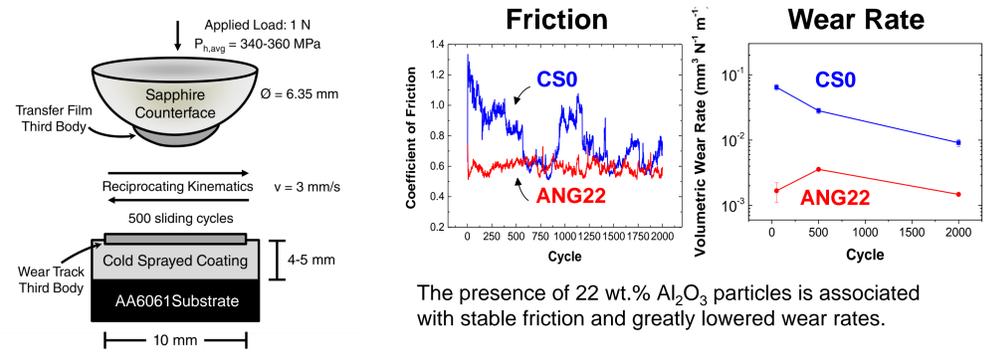


The pure Al coating consolidated into a dense microstructure with <2% porosity.



A proportion of the Al<sub>2</sub>O<sub>3</sub> particles were recovered to form a uniform Al-Al<sub>2</sub>O<sub>3</sub> microstructure.

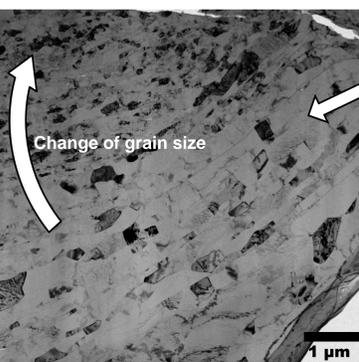
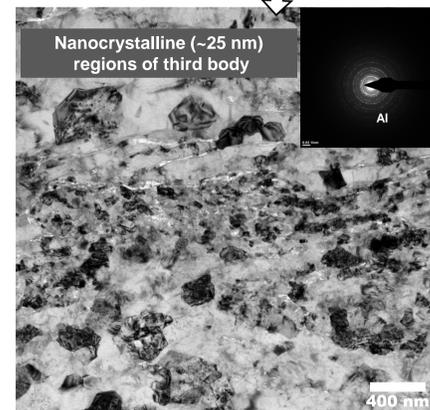
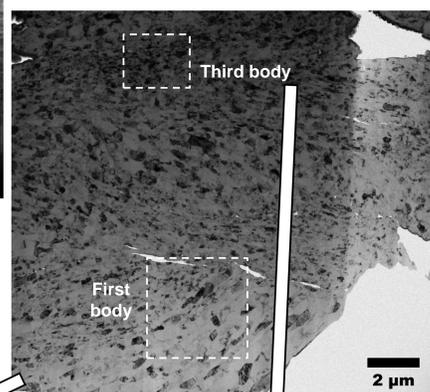
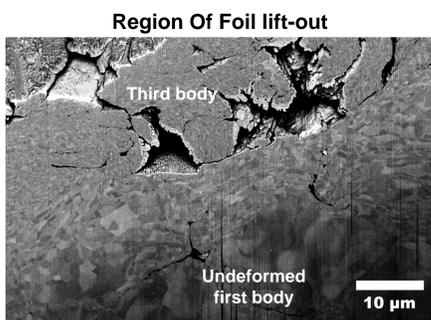
## DRY SLIDING WEAR EXPERIMENTS



The presence of 22 wt.% Al<sub>2</sub>O<sub>3</sub> particles is associated with stable friction and greatly lowered wear rates.

## MICROANALYSIS: BRIGHT FIELD TEM AND ELEMENTAL MAPPING

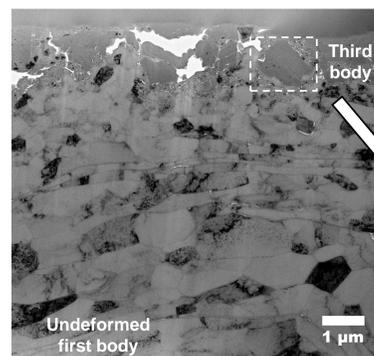
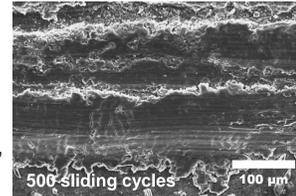
### CS0: 100 wt.% Al



Grain size gradient: transition from third body to first body

**Surface analysis of wear tracks reveals:**

- CS0 shows evidence of adhesion and smearing
- ANG22 forms smooth, coherent tribofilms



**Low magnification TEM reveals:**

- CS0 : subsurface deformation runs very deep, making gradients of grain size
- ANG22 : sharp transition from "large" grained Al to third body

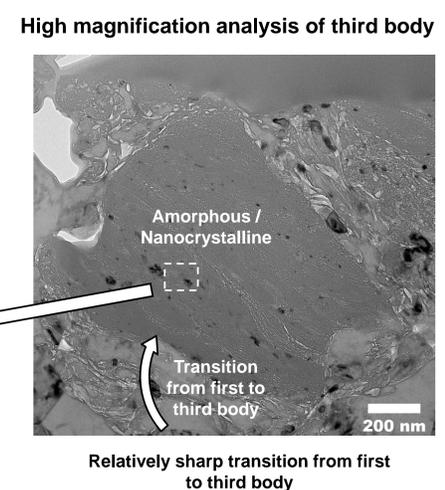
**High magnification TEM of third bodies reveals:**

- CS0 Mixture of grain sizes down to nanocrystalline
- ANG22 primarily amorphous material with very small Al grains mixed in

**Nanoindentation hardness of third bodies:**

- CS0 ~1.5 GPa
- ANG22 ~3.8 GPa

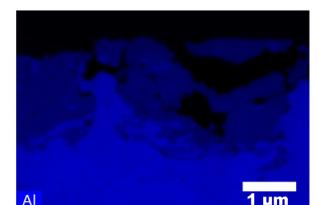
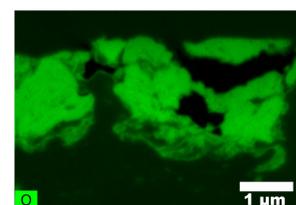
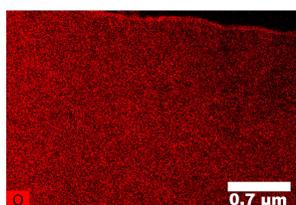
### ANG22: Al-22 wt.% Al<sub>2</sub>O<sub>3</sub>



Relatively sharp transition from first to third body

**EDS mapping reveals:**

- CS0 : Moderately elevated oxygen levels in third body
- ANG22 Third body oxygen levels nearly as high as α-Al<sub>2</sub>O<sub>3</sub>



## ACKNOWLEDGEMENTS AND REFERENCES

- [1] G.W. Stachowiak and A.W. Batchelor, Engineering Tribology (Elsevier, Amsterdam, 2005).
- [2] J.M. Shockley, H. Strauss, R.R. Chromik, N. Brodusch, R. Gauvin, E. Irissou, J.-G. Legoux / Surface and Coatings Technology 215 (2013) pp. 350-356.
- [3] J.M. Shockley, S. Descartes, E. Irissou, J.-G. Legoux, R. R. Chromik / Tribology Letters 54 (2014) pp. 191-206.
- [4] S. Descartes, C. Desrayaud, E. F. Rauch / Materials Science and Engineering A 528 (2011) pp. 3666-3675.

## CONCLUSIONS

FIB lift-out and TEM have revealed details of the microstructural changes occurring in third body material after dry sliding wear of cold sprayed Al and Al-Al<sub>2</sub>O<sub>3</sub>. The presence of 22 wt.% Al<sub>2</sub>O<sub>3</sub> particles led to the formation of a largely amorphous, heavily oxidized third body layer. This was much harder than the nanocrystalline third body material of the pure Al and protected the underlying material from damage.